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ENERGY AND TIME BETA RAY SPECTRA OF FISSION PRODUCTS OF U235 BY FISSION NEUTRONS AND U236 BY 14 MEV NEUTRONS Robert B. Heller

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WSEG Research Memorandum No. 19

ENERGY AND TIME BETA RAY SPECTRA OF FISSION PRODUCTS OF U²⁹⁵ BY FISSION NEUTRONS AND U²⁹⁶ BY 14 MEV NEUTRONS

Robert B. Heller

16 February 1961

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EMERGY AND TIME BETA RAY SPECTRA OF FISSION PRODUCTS OF U295 BY FISSION NEUTRONS AND U296 BY 14 NEW NEUTRONS

INTRODUCTION

The primary purpose of this memorandum is to provide a practical estimate of the beta ray spectrum from fission products at short times after fission.

The machine program developed to furnish this information automatically provides the spectrum for later times at very little additional effort, together with the distribution of beta radiation by specific nuclides.

This information has been developed and is presented in this memorandum for 14 MEV neutron fissioning of U^{238} and also for U^{238} fissioned by fission neutrons.

RETHOD

The disintegration rate $\beta_j(t)$, for the j^{th} fission fragment of a chain was generated by solving the differential equation for the decay chain and computing the activity $\beta_j(t)$ at a series of times t.

^{1/} Acknowledgement is made of the valuable assistance given to me by Dr. George E. Pugh, Miss Joanna Frawley, Mrs. Elaine Marcuse, and Mrs. Juanita Price in the development and calculations needed for this paper.

 $\beta_j(t)$ was then multiplied by a function $\rho_j(E)$ which gives the probability that the decay yields a beta ray with kinetic energy E. The product $\beta_j(t)\rho_j(E)dE$ gives the number of beta rays at a given energy and time from the j^{th} isotope, in the energy range between E and E + dE.

The product $\beta_j(t)\rho_j(E)$ was summed over all known or postulated members of a specific fission chain with mass number A. This yields

$$\sum_{j} \beta_{j}(t) \rho_{j}(E). \tag{1}$$

If the above expression is then summed over all fission chains with mass numbers from about 72 to 162, the complete energy and time function is obtained for the beta activity from fission.

$$\beta(E,t) = \sum_{A} \sum_{j} \beta_{j}(t) \rho_{j}(E) \qquad (2)$$

INPUT DATA

The complete summation expressed in equation (2) requires input data of two general categories; they are:

 \underline{a} . The initial fission abundance of the isotopes by chain mass number A and by charge distribution Z within the chain A. This, plus the decay time constants, suffice to calculate $\beta_j(t)$.

<u>b</u>. The beta ray and point energy E_0 plus the forbidden degree of the beta transition. These factors enable the calculation of the probability function $\rho_4(E)$.

neutrons actually used in this development were experimentally determined and reported in Los Alamos Report, LA 1997. The solid line in Figure 1 represents data taken from LA 1997. The dashed line fills in the mass yields below A = 90. These were taken from the work of J. G. Cuninghame and smoothed into the Los Alamos results. Figure 2 gives the fission spectrum neutron mass yield from U^{295} fission. This curve was synthesized by altering the thermal neutron yield so that the valley fragment yields were increased to lie between capsule and 1 MEV neutron fission yields, the double peaks suppressed to lie between the known 14 MEV and thermal yields, and the wings opened to half the difference between the 14.7 MEV and thermal yields.

The distribution of nuclear charge in fission occurring within a given mass chain has been, and remains, a somewhat uncertain theoretical experimental problem.2/

^{1/} J. G. Cuninghame, The Mass Yield Curve for Fission of Natural Uranium by 14 MEV Neutrons, J. Inorg. Nucl. Chem. 5, 1 (1957).

^{2/} For a more complete discussion see L. E. Glendenin, D. C. Coryell, and R. R. Edwards, Paper 52, p. 489, Radio Chemical Studies, The Fission Products Book 1, McGraw-Hill.

The postulate of equal charge displacement was used in this study to obtain the most probable division of charge between the two fission fragments of U^{235} . The most probable charge division leads to equal $(Z_A - Z_p)$ values for the two fission fragments, where Z_p is the most probable charge for the fragment and Z_A the hypothetical charge of maximum stability for a given mass chain number A.

It was assumed that the distribution of charge around the most probable charge Z_p is symmetrical. The fraction of the total initial chain yield in any chain number Z is calculated from its $Z-Z_p$ value using Figure 52.2 on page 495 of footnote 2, page 3 of this paper.

The equal charge displacement and symmetrical distribution around this most probable charge appears reasonable in view of the experimental agreement for the observed shielded nuclides Br⁸², Rb⁸⁶, Cs¹³⁶ and Xe¹³⁵. The fraction of the total initial number of U²³⁵ fission products in various chain positions was determined using the above-procedure.

The most probable nuclear charge division defines, for primary fission products of a specific mass chain, the hypothetical Z_p value around which other initial members of the chain are distributed according to the various charge distribution postulates, e.g., for the equal charge displacement postulate the predicted most probable nuclear charges for primary products of masses 82 and 86 are 32.4 and 34.0.

The decay constants of more than 50 percent of the possible 412 fission fragments have not been experimentally observed nor investigated. The decay schemes used by Bolles and Ballou2/ were used in the computations described herein for U235. Some 202 nuclides half lives in these decay schemes have not as yet been observed but calculated values were used.

In the case of the decay constants and independent yields of U238 by 14 MEV neutrons the values used were those calculated by P. J. Dolan3. In these calculations, the most probable charge for a fission fragment of given mass was determined according to the theory of Pappas as extended by Ford and Gilmore 5/

It was necessary to assign a fraction of parent activity going to each isomer where a chain contained an isomeric pair.

^{1/} Latest data from D. Strominger, J. M. Hollander, and G. T. Seaborg, Rev. Mod. Phys. 30, 585 (1958).

^{2/} R. C. Bolles and N. E. Ballou, <u>Calculated Activities and Abundances of U²³⁵ Fission Products</u>, U.S. Radiological Defense Laboratories, <u>USNRDL-456</u>, 30 August 1956.

3/ P. J. Dolan, <u>Gamma Spectra of U²³⁸ Fission Products at Various Times after Fission</u>, <u>Defense Atomic Support Agency</u>

Report 526, May 1959.

^{4/} A. C. Pappas, A Radiochemical Study of Fission Yields in the Region of Shell Perturbations on the Effects of Closed Shells in Fission, Laboratory for Nuclear Science, Massachusetts Institute of Technology, Technical Report No. 63, 15 September 1953.

^{5/} G. P. Ford and J. S. Gilmore, Mass Yields From Fission By Neutrons Between Thermal and 14.7 MEV, Los Alamos Scientific Laboratory of University of California, LA 1997, February 1956.

Most of these proportions were known from experimental determination. When lacking, isomeric activity was estimated from measured fission yield of one isomer and the total chain yield. Arbitrary ratios of 50-50 of the parent activity of Rb⁹¹, In¹¹⁷, and Cs¹¹⁹ were assigned to each daughter isomer.

THE BETA END POINT ENERGIES

Available experimentally determined beta ray end point kinetic energies were assigned to their corresponding isotopes.

For a rough prediction of the total beta decay energy Q_B of unknown nuclides or beta activity too short to have been determined, the procedure suggested by Coryell was used. (See Table I for the calculated results.) Any loss of this available energy Q_B to gamma ray transitions in the short half life unknown decays was ignored. By so doing, this report can only hope to develop an approximate upper limit for the high energy portion of the beta spectrum and for times less than 30 seconds after fission.

ALLOWED AND FORBIDDEN SPECTRA

In general, where experimentation classified the transitions as allowed or forbidden, the appropriate energy-shaping expression or correction factors were used. When experimental

^{1/} C. D. Coryell, Beta Decay Energetics, Annual Review of Nuclear Science, Vol. 2, 1953, p. 331, (UNCLASSIFIED).

results were lacking, the forbiddenness was chosen to agree with the Ft values of Feingold or the classification based upon the nuclear shell structure of M. G. Mayer. $\frac{2}{3}$

LIMITATIONS OF THE HALF LIFE, END POINT ENERGY AND FORBIDDENNESS INPUT DATA

While it is common practice to assume 100 percent beta transition between ground states whenever experimental information is unavailable, studies by Perkins and King have shown that this simplification may lead to errors in both the beta and gamma radiation associated with fission. In their procedure, which is adjusted to be consistent with the experimentally measured total gamma energy from all the fission product decay, a single "effective" beta and gamma transition is used and adjusted to account for the mass difference between parent and daughter.

This sharing of the total energy between effective beta and gamma would result in somewhat lower beta and point energies than that used in this study. In addition, if the single "effective" beta and gamma transition recipe for unknown decays were used, a readjustment of half lives towards smaller values would result.

- 7 -

^{1/} A. M. Feingold, Table of Ft Values in Beta Decay, Review of Modern Physics, Vol. 23, 1951, pp. 10-18.

^{2/} M. G. Mayer and S. A. Moszkowski, <u>Nuclear Shell Structure and Beta Decay</u>, I. Odd A Nuclei, Review of Mcdern Physics, Vol. 23, 1951, pp. 315-321.

^{3/} L. W. Nordheim, <u>Nuclear Shell Structure and Beta Decay II</u>. <u>Even A Nuclei</u>, <u>Review of Modern Physics</u>, Vol. 23, 1951, pp. 322-327.

^{4/} R. W. King and J. F. Perkins, <u>Inverse Beta Decay and the Two Component Neutrons</u>, Phys. Rev. Vol. 112, No. 3, pp. 903-960, November 1, 1958.

In the near future it is planned to investigate the effect on our results of incorporating new data for the unknown decays, based upon the procedure suggested by King and Perkins.

INPUT DATA TABULATION

Table II displays all the input data used in carrying out the calculations. The tabulated data, from left to right, is: λ (decay constant), $F_{U^{235}}$ and $F_{U^{238}}$ (initial fission abundance), E_{0} (beta end point energy), Δ (the fraction going by beta decay), and symbols 0 for allowed and 1 for forbidden spectra. The values of λ , $F_{U^{235}}$, $F_{U^{238}}$, and E_{0} are printed directly from a computer tabulation. The last two digits represent the power of 10 by which the remaining digits, treated as an eight place decimal, are to be multiplied. 51 in this position represents 10^{1} , 50 represents 10^{0} , 49 represents 10^{-1} , etc.

Many of the decay schemes contain disintegrations yielding beta, gamma and neutrons. The concern in this report is only with isotopes yielding beta rays. In order to maintain the proper rate of change and growth for the isotopes in these chain decay schemes and avoid unnecessary complication of the program, a simple procedure was used which includes transitions due to all emissions. However, in the computation of $\beta_j(t)$, each member of a chain was assigned a multiplication operator Δ , expressing the percent of the decay that proceeds by beta emission. Where only isomeric gamma decays or neutron decays WSEG RM 19 -8

occur, Δ is taken as zero. By assigning zero and end-point beta energy to non-beta transitions, we are assured of their not being calculated or tabulated either in the end product of the $\beta_j(t)\rho_j(E)$ calculation or in the machine summation of $\beta_j(t)$, which tests for non-zero end point energy.

TABULATION OF FORMULAE

There is an assigned initial abundance to every possible isotope resulting from fission. As time proceeds each isotope will decay in abundance, characteristic of its decay constant. In addition, the instantaneous amount of each isotope may be increased due to the decay of the members of the chain.

The machine program used to analyze the decay of the fission fragments and compute $\beta_j(t)$ was based upon the following differential equation:

$$\frac{dA_{j}}{dt} + \lambda_{j}A_{j} = A_{j-1} \times \lambda_{j-1} , \qquad (3)$$

where $\beta_j(t) = \lambda_j A_j(t)$

and $A_j(t)$ is the amount of the j^{th} isotope at time t,

where j=1 . . . i_0 . The time differential expresses the rate of change of an isotope (A_j) with decay constant λ_j , in terms of all previous members of a chain and their decay constants.

We assume a solution of the form

$$A_{j}(t) = \sum_{i=1}^{i=j} \gamma_{ij} e^{-\lambda_{i}t}$$
 (4)

where the constants γ_{ij} are to be determined from the following recursion relationships:

$$\gamma_{i,j} = \left(\frac{\lambda_{j-1}}{\lambda_{j}-\lambda_{i}}\right) \gamma_{i,j-1} \quad \text{for } i < j, \text{ and}$$
 (5)

$$\gamma_{jj} = A_{j}(0) - \sum_{i=1}^{j-1} \gamma_{ij}$$
 (6)

If a fission fragment mass chain A has a nuclear charge distribution from Z to (Z+n), the total instantaneous chain activity is

$$\sum_{j=Z}^{Z+n} \beta_j(t) . \tag{7}$$

The total activity at $t=t_1$ from all fission chains (A= 72 to 162) used in this study is

$$\sum_{A=72}^{162} \sum_{j=Z}^{Z+n} \beta_{j,A}(t_1). \tag{8}$$

THE PROBABILITY FUNCTION $\rho(E)$

 $\rho(E)dE$ is the probability that a beta emitted from the $j^{\mbox{th}}$ isotope has an energy between E and E+dE, and is of the form:

$$\rho_{j}(E) = \frac{E(E^{2} - 1)^{\frac{1}{2}} (E_{0} - E)^{2} F(Z + 1, E) \cdot g^{2} \xi}{\int_{1}^{E_{0}} E(E^{2} - 1)^{\frac{1}{2}} (E_{0} - E)^{2} F(Z + 1, E) \cdot g^{2} \xi dE}$$
(9)

where

E = beta energy in rest mass (m_oc²) units

 $E_0 = beta end point energy in <math>m_0c^2$ units

F(Z + 1,E) = energy correction term due to the Coulomb

distortion of an electron wave amplitude in
the Coulomb field of the nucleus 1/

g = Fermi's fundamental coupling constant

$$\xi = \left| C_{V} \right|^{2} \cdot \left| \langle 1 \rangle \right|^{2} + \left| C_{A} \right|^{2} \cdot \left| \langle \sigma \rangle \right|^{2}.$$

A coefficient in the general expression indicating a nuclear matrix element mixture of vector and pseudo-vector coupling.

If it can be assumed that the nuclear matrix element expression in (9) is not a function of the beta or neutrino energy, then (9) reduces to

$$\rho_{j}(E) = \frac{E(E^{2}-1)^{\frac{1}{2}} (E_{0}-E)^{2} F(Z+1,E)}{E_{0}}$$

$$\int E(E^{2}-1)^{\frac{1}{2}} (E_{0}-E)^{2} F(Z+1,E) dE$$
(10)

which covers in our study the allowed and once forbidden transitions having allowed shapes. To allow for isotopes having forbidden shapes, $\rho_1(E)$ is modified as follows:

^{1/} Values for this Coulomb Function were calculated using The Table of the Gamma Function for Complex Arguments, U.S. Bureau of Standards.

$$\rho_{j}(E) = \frac{E(E^{2} - 1)^{\frac{1}{2}} (E_{0} - E)^{2} F(Z + 1, E) \cdot \{(E^{2} - 1) + (E_{0} - E)^{2}\}^{\alpha}}{\int_{E}^{E_{0}} E(E^{2} - 1)^{\frac{1}{2}} (E_{0} - E)^{2} F(Z + 1, E) \{(E^{2} - 1) + (E_{0} - E)^{2}\}^{\alpha} dE}$$
(11)

where α is the degree of forbiddenness. In this study $\alpha=0$ covers all allowed and once forbidden transitions having allowed shapes. $\alpha=1$ is used to cover other once or twice forbidden transitions. The energy expression in the brackets is the well-known p^2+q^2 electron and neutrino momentum correction term in m_0c^2 units.

FINAL EXPRESSION

For the member j = Z of chain A in equation (11) $\beta_{Z,A}(E,t) dE = \beta_{Z,A}(t) \cdot \Delta \cdot \rho_{Z}(E) dE \qquad (12)$

 $\beta_{ZA}(t)$ is given by equation (5), and Δ is the fraction of the decay that goes by a beta ray.

RESULTS

Some selected results of this analysis, as carried out on the IBM 650, are plotted in Figure 3 for U²³⁵ and Figure 4 for U²⁸⁸. These two figures give the number of beta rays per fission per energy interval for any specific energy. The short time contribution from highly energetic short-lived isotopes is quite apparent.

^{1/} The complete calculation for expression (12) for all values of time is on file in IDA/WSEG and is available upon request.

Figures 5(a) through 5(q) and 6(a) through 6(q) present some processed data, the percent of total beta energy per fission per isotope versus time. All fission chains and their constituent members are included for U^{235} and U^{236} .

Figures 7 and 8 present for U^{235} and U^{238} the total beta activity per fission summed over all energy versus time.

Figures 9 and 10 present the total beta energy released per fission per second versus the kinetic energy of the beta rays from fission fragment of U^{235} and U^{238} .

Figures 11 and 12 present the percent of the total beta activity per fission for a few selected times versus the kinetic energy of the beta rays from U^{238} and U^{235} fission fragments.

Figures 13 and 14 present the percent of the total beta energy per interval for a few selected times versus the kinetic energy of the beta rays from $U^{23.5}$ and $U^{23.6}$ fission fragments.

Figure 15 compares the result of this study with its assumption of all beta transition to ground state for short half-life unknowns, to those of Cameron and King. 2/ While

^{1/} A. G. W. Cameron, Chalk River Project - 690, 1957.
2/ R. W. King and J. F. Perkins, Inverse Beta Decay and the Two-Component Neutrons, Phys. Rev., Vol. 112, No. 3, pp. 963-966, November 1, 1958.

this study used fission spectrum neutrons in U²³⁵ fission, the expected difference with thermal neutrons should be very small. It is apparent from Figure 15 that the King and Perkins assumption—of peing shared by beta transitions to nonground levels as well as gamma from the excited levels to ground—yields a somewhat lower number of high energy betas. The results of this study agree very well with those based—upon Cameron's total disintegration energies for the unknown decays.

TABLE I

CALCULATED BETA END POINT ENERGIES &

 $\underline{\mathbf{z}}$ Two primary sources were used in these calculations. $\mathbf{z}_{\mathbf{A}}$ values were taken from Coryell and Sugarman.

Radiochemical Studies: The Fission Product Book 1, McGraw-Hill, page 494, Figure 51.1 and Table 52.10, page 512.

 B_A , δ_A , and ϵ_A , from Table II (page 325), Table IV (page 331) and Table I (page 320), respectively, of Annual Review of Nuclear Science, Vol. II, 1953.

The basic equations are:

- (1) $Q_B = B_A(Z_A Z 0.5) \pm \delta_A$ for (A even).
- (2) $Q_B = B_A(Z_A Z 0.5) \pm \epsilon_A$ for (A odd).

TABLE I

CALCULATED BETA END POINT ENERGIES

A	z	ZA	BA	A even	A odd	Use eq.	z _A - z5	$B_A(Z_A - Z5)$	Q ^B (MEV)	
72	28 29	32	2.45	2.82		-+	3·5 2·5	8.58 6.12	5.76 8.94	
73	28 29 30	32.3	2.42		-•3	- + -	3.8 2.8 1.8	9.20 6.78 4.36	9.50 6.44 4.60	В
74	28 29 30	32.7	2.38	2.38		- + -	4.2 3.2 2.2	10.00 7.62 5.24	7.17 10.45 2.41	
75	29 30 31	33	2.36		-•3	+ - +	3.5 2.5 1.5	8.26 5.90 3.54	7.90 6.20 3.21	0
76	29 30	33.4	2.34	2.84		+	3.9 2.9	9.13 6.79	11.97 3.95	
77	29 30 31 32 33	33.8	2.31		3	+ - + -	4.3 3.3 2.3 1.3 0.3	9.93 7.62 5.31 3.00 0.69	9.65 7.98 5.03 3.30 .59	2
78	30 31	34.2	2.29	2.86		- +	3.7 2.7	8.47 6.18	5.61 9.04	
79	30 31 32	34.6	2.27		 3	- + -	4.1 3.1 2.1	9.31 7.04 4.77	9.6: 6.7 ¹ 5.0	4
80	30 31 32	35	2.24	2.86		- + -	4.5 3.5 2.5	10.08 7.84 5.60	7.22 10.70 2.74	
81	31 32 33 34	35.5	2.21		3 3 1	+ - + -	4.0 3.0 2.0 1.0	8.84 6.63 4.42 2.21	8.51 6.93 4.32 2.33	3
82	31 32 33	36	2.18	2.87		+ - +	4.5 3.5 2.5	9.81 7.63 5.45	12.68 4.76 8.32	

TABLE I (Continued)

<u>A</u>	<u>z</u>	ZA	BA	A even	€ ¥	Use eq.	$\frac{z_A - z5}{2}$	$\frac{B_{\mathbf{A}}(\mathbf{Z}_{\mathbf{A}}-\mathbf{Z}5)}{2}$	q ^B (ME	<u>v)</u> 8.51
83	32 33 34	36.2	2.16		3 1 1	+	3.8 2.8 1.8	8.21 6.05 3.89		5.95 3.99
84	32 33	36.7	2.14	2.88		- +	4.2 3.2	8.99 6.85	6.11 9.73	
85	32 33 34 36	37	2.12		3 1 1	- + -	4.5 3.5 2.5 0.5	9.54 7.42 5.30 1.06		9.84 7.32 5.40 1.16
86	32 33 34 35	37.5	2.09	2.88		- + - +	5.0 4.0 3.0 2.0	10.45 8.36 6.27 4.18	7.57 11.24 3.39 7.06	
87	33 34 36	2.06			1 1 1	+ - +	4.5 3.5 1.5	9.27 7.21 3.09		9.17 7.31 2.99
88	34 35 36	28.5	2.03	2.88		- + -	4.0 3.0 2.0	8.12 6.09 4.06	5.24 8.97 1.18	
89	34 35 36	39	2.01		1 1 1	- + -	4.5 3.5 2.5	9.04 7.04 5.02		9.14 6.94 5.12
90	34	39.4	1.99	2.88		-	4.9	9.75	6.87	
91	35 36 37 39	39.9	1.97		1 1 1 +.4	+ - + +	4.4 3.4 2.4 0.4	8.67 6.70 4.73 0.79		8.57 6.80 4.63 1.19
92	35 36+ 37	40.3	1.96	2.88		+ - +	4.8 3.8 2.8	9.41 7.45 5.49	12.29 4.57 8.37	
93	36 37 38	40.7	1.94		1 1 1	- + -	4.2 3.2 2.2	8.15 6.21 4.27		8.25 6.11 4.37
94	36 37 38	41.1	1.92	2.88		- +	4.6 3.6 2.6	8.83 6.91 4.99	5.95 9.79 2.11	

TABLE I (Continued)

A	<u>z</u>	z _A	BA	A even	A odd ∈ A	Use eq.	z _A -z5	$\frac{B_{A}(Z_{A}-Z5)}{B_{A}(Z_{A}-Z5)}$	QB(MEV)
95	36 37 38 39 41	41.6	1.90		1 1 1 +.4 +.4	- + - +	5.1 4.1 3.1 2.1 0.1	9.69 7.79 5.89 3.99 0.19	9•79 7•69 5•99 4•39 •59
96	37 38 39	42.1	1.88	2.87		÷ - +	4.6 3.6 2.6	8.65 6.77 4.89	11.52 3.90 7.76
97	37 38 39 41	42.6	1.86		1 1 +.4 +.4	+ - + +	5.1 4.1 3.1 1.1	9.49 7.63 5.77 2.05	9.39 7.73 5.17 2.45
98	38 39 40 41	43	1.85	2.85		- + - +	4.5 3.5 2.5 1.5	8.32 6.48 4.62 2.78	5.47 9.33 1.77 5.63
99	39 40 43	43.5	1.83		- 1 - 1 - 1	+ - +	4.0 3.0 0.0	7.32 5.49 0	7.72 5.09 .4
100	39 40 41	3434	1.81	2.84		+ - +	4.5 3.5 2.5	8.14 6.34 4.52	10.98 3.50 7.36
101	39 40 41	44.4	1.79		+•14	÷ - +	4.9 3.9 2.9	8.77 6.98 5.19	9.17 6.58 5.59
102	40 41 42	44.8	1.78	2.82		+	4.3 3.3 2.3	7.65 5.87 4.09	4.83 8.69 1.27
103	40 41 42	45.2	1.76		- jt - jt - jt	+	4.7 3.7 2.7	8.27 6.51 4.75	7.87 6.91 4.35
104	40 41 42	45.6	1.75	2.80		+	5.1 4.1 3.1	8.92 7.18 5.42	6.12 9.98 2.62

TABLE I (Continued)

<u>A</u>	z	Z _A	BA	A even δ _A	A odd €A	Use eq.	z _A - z5	$\underline{B_{\mathbf{A}}(Z_{\mathbf{A}}-Z-5)}$	Q ^B (MEV)
105	41 42 43 45	46.0	1.73		. 4 . 4 . 4	+ - + +	4.5 3.5 2.5 0.5	7.78 6.06 4.32 .86	8.18 5.66 4.72 1.26
106	41 42	46.4	1.72	2.77		+ - +	4.9 3.9 2.9	8.43 6.71 4.99	11.20 3.94 7. 76
107	41 42	56.8	1.70		.4 .4 .4	+ - +	5•3 4•3 3•3	9.01 7.31 5.61	9.41 6.91 6.01
108	42 43 44	47.2	1.68	2.74		+	4.7 3.7 2.7	7.90 6.22 4.54	5.16 8.96 1.80
109	42 43 44 45	47.5	1.67		.4	- + - +	5.0 4.0 3.0 2.0	8.35 6.68 5.01 3.3 ¹ 4	7.95 7.08 4.61 3.54
110	42 43 44 45	47.8	1.66	2.72		- + - +	5.3 4.3 3.3 2.3	8.80 7.14 5.48 3.82	6.08 9.86 2.76 6.54
111	43 44 45	48.1	1.65		.4 .4 .2	+ - +	4.6 3.6 2.6	7·59 5·94 4·29	7.99 5.54 4.49
112	43 44 45	48.4	1.64	2.69		+ - +	4.9 3.9 2.9	8.04 6.40 4.76	10.73 3.71 7.45
113	44 45 46	48.7	1.62		.4 .2 0	- + -	4.2 3.2 2.2	6.80 5.18 3.56	6.40 5.38 3.56
114	44 45 46 47	49.0	1.61	2.66		- + - +	4.5 3.5 2.5 1.5	7.24 5.64 4.02 2.41	4.58 8.30 1.36 5.07

TABLE I (Continued)

<u>A</u>	<u>z</u>	z _A	BA	A even	A odd € A	Use eq.	z _A - z5	$\underline{\mathbf{B}_{\mathbf{A}}(\mathbf{Z}_{\mathbf{A}} -\mathbf{Z}5)}$	Q ^B (MEV)
115	44 45 46 48 49	49.3	1.60		0 .2 0 0	- + - - +	4.8 3.8 2.8 0.8 -0.2	7.68 6.08 4.48 1.28 32	7.68 6.28 4.48 1.28
116	45 46	49.6	1.59	2.62		+	4.1 3.1	6.52 4.93	9.14 2.31
117	45 46 47 48 49	49.9	1.58		.2 0 0 0	+ - + - +	4.4 3.4 2.4 1.4 0.4	6.95 5.37 3.79 2.21 .63	7.15 5.37 3.79 2.21 1.13
118	45 46 47 48	50.2	1.57	2.58		+ - + -	4.7 3.7 2.7 1.7	7.38 5.81 4.24 2.67	9.96 3.23 6.82 .09
119	45 46 47 48 49	50•5	1.56		.2 0 0 0	+ - + -	5.0 4.0 3.0 2.0 1.0	7.80 6.24 4.68 3.12 1.56	8.00 6.24 4.68 3.12 2.06
120	46 47 48 49	50.8	1.54	2.55		- + - +	4.3 3.3 2.3 1.3	6.62 5.08 3.54 2.00	4.07 7.63 .99 4.55
121	46 47 48 49 50	51.1	1.53		0 0 0 •5	+ - + -	4.6 3.6 2.6 1.6 0.6	7.04 5.51 3.98 2.45	7.04 5.51 3.98 2.95
122	46 47 48 49	51.4	1.52	2.51		+ - +	4.9 3.9 2.9 1.9	7.45 5.93 4.41 2.89	4.94 8.44 1.90 5.40
123	47 48 49	51.7	1.51		0 0 .5	+ - +	4.2 3.2 2.2	6.34 4.83 3.32	6.34 4.83 3.82

TABLE I (Continued)

A	z	Z _A	BA	A even	A odd € A	Use eq.	Z _A -Z5	$B_A(Z_A - Z5)$	QB(MEV)
124	47 48 49	52.0	1.51	2.47		+ - +	4.5 3.5 2.5	6.80 5.28 3.78	9.27 2.81 6.25
125	47 48	52.3	1.50		0 0 •5	+ - +	4.8 3.8 2.8	7.20 5.70 4.20	7.20 5.70 4.70
126	48 49 50	52.6	1.49	2.40		- + -	4.1 3.1 2.1	6.11 4.62 3.13	3.71 7.02 .73
127	48 49 50 52	52.9	1.48		0 •5 0 0	+	4.4 3.4 2.4 0.4	6.51 5.03 3.55 .59	6.51 5.53 3.55 .59
128	48 49 50	53.2	1.47	2.35		- + -	4.7 3.7 2.7	6.91 5.44 3.97	4.56 7.79 1.62
129	48 50 51 52	53.5	1.46		•5 0 4 0	+ + +	4.0 3.0 2.0 1.0	5.84 4.38 2.92 1.46	6.34 4.38 2.52 1.46
130	49 50 51	53.9	1.46	2.29		÷ - +	4.4 3.4 2.4	6.42 4.96 3.50	8.71 2.67 5.79
131	49 50 51 52 53 54	54.2	1.45		•5 0 ••4 0 0	+ - + -	4.7 3.7 2.7 1.7 0.7 -0.3	6.81 5.36 3.92 2.46 1.01 44	7.31 5.36 3.52 2.46 1.01
132	50 51	54.5	1.44	2.24		+	4.0 3.0	5.76 4.32	3.52 6.56
133	50 51 52	54.9	1.43		-• 1	+	4.4 3.4 2.4	6.29 4.86 3.43	6.29 4.46 3.43

TABLE I (Continued)

<u>A</u>	<u>z</u>	Z _A	B _A	A even	A odd EA	Use Eq.	z _A - z5	$\underline{B_{\mathbf{A}}(Z_{\mathbf{A}}-Z5)}$	Q ^B (MEV)	Σ
134	51 52	55.3	1.42	2.19		<u>+</u>	3.8 2.8	5.40 3.98	.7•59 1•79	
135	51 52	55.7	1.41		4	+	4.2 3.2	5.92 4.51	í	5.52 4.51
136	51 52	56.1	1.40	2.14		+	4.6 3.6	6.44 5.04	8.58 2.90	
137	52	56. 5	1.39		0	-	4.0	5.56	5	5.56
138	52 53	57.0	1.37	2.09		- +	4.5 3.5	6.165 4.80	4.07 6.89	
139	53 54 55	57.5	1.36		0 0 0	+ - +	4.0 3.0 2.0	5.44 4.08 2.72		5.44 4.08
140	53 54 55	58.0	1.35	2.05		+ - +	4.5 3.5 2.5	6.075 4.72 3.38	8.13 2.67 5.43	
141	54 55	58.5	1.34		0	-	4.0 3.0	5.36 4.02	í	5.36 4.02
142	54 55 56 57	59.0	1.33	2.0		- + - +	4.5 3.5 2.5 1.5	5.98 4.65 3.32 2.00	3.98 6.65 1.32 4.00	
143	55 56 57	59•5	1.32		0 0 •35	+ - +	4.0 3.0 2.0	5.28 3.96 2.64		5.28 3.96 2.99
144	55 56 57	59.9	1.31	1.97		+ - +	4.4 3.4 2.4	5.76 4.45 3.14	7.73 2.48 5.11	
145	55 56 57	60.4	1.30		0 0 •35	+ - +	4.9 3.9 2.9	6.37 5.07 3.77	-	5.37 5.07 4.12
146	56 57	60.9	1.28	1.93		- +	4.4 3.4	5.63 4.35	3.70 6.28	

TABLE I (Continued)

<u>A</u>	z	Z _A	B _A	A even	A odd EA	Use eq.	Z _A - Z5	$B_{A}(Z_{A} - Z5)$	QB(MEV)
147	56 57 58 59 60	61.4	1.27		0 •35 0 •35 0	- + - +	4.9 3.9 2.9 1.9	6.22 4.95 3.68 2.41 1.14	6.22 5.30 3.68 2.76 1.14
148	57 58 59	61.9	1.26	1.89		+ - +	4.4 3.4 2.4	5.54 4.28 3.02	7.43 2.39 4.91
149	57 58 59	62.3	1.25		•35 0 •35	+ - +	4.8 3.8 2.8	6.00 4.75 3.50	6.35 4.75 3.85
150	58 59	62.6	1.25	1.86		- +	4.1 3.1	5.12 3.88	3.26 5.74
151	58 5 9	62.9	1.24		o •35	- +	4.4 3.4	5.45 4.22	5.45 4. 57
152	58 59 60 61	63.2	1.24	1.84		- + - +	4.7 3.7 2.7 1.7	5.83 4.59 3.35 2.11	3.99 6.43 1.51 3.95
153	59 60 61	63.5	1.23		•35 0 •35	+ - +	4.0 3.0 2.0	4.92 3.69 2.46	5.27 3.69 2.81
154	59 60 61	63.9	1.22	1.80		+ - +	4.4 3.4 2.4	5·37 4·15 2·93	7.17 2.35 4.73
155	59 60 61	64.3	1.21		•35 0 •35	+ - +	4.8 3.8 2.8	5.81 4.60 3.39	6.16 4.60 3.74
156	60 61	64.6	1.21	1.77		- +	4.1 3.1	4.96 3.75	3.19 5.52
157	60 61 62	64.8	1.20		0 •35 0	- + -	4.3 3.3 2.3	5.16 3.96 2.76	5.16 4.31 2.76

TABLE I (Continued)

<u>A</u>	z	ZA	BA	A even	A odd A	Use Eq.	z _A - z5	$\frac{B_{\mathbf{A}}(Z_{\mathbf{A}}-Z5)}{}$	QB(MEV)
158	60 61 62	65.1	1.20	1.74		÷	4.6 3.6 2.6	5.52 4.32 3.12	3.78 6.06 1.38
159	61 62	65.3	1.20		•35 0	+ -	3.8 2.8	4.56 3.36	4.91 3.36
160	65.5 62 63	5	1.19	1.72		+ - +	4.0 3.0 2.0	4.76 3.57 2.38	6.48 1.85 4.10
161	62 63	65.7	1.19		0.2	- +	3.2 2.2	3.81 2.62	3.81 2.82
162	62 63 64	65.9	1.19	1.70		+	3.4 2.4 1.4	4.05 2.86 1.67	2.35 4.56 03

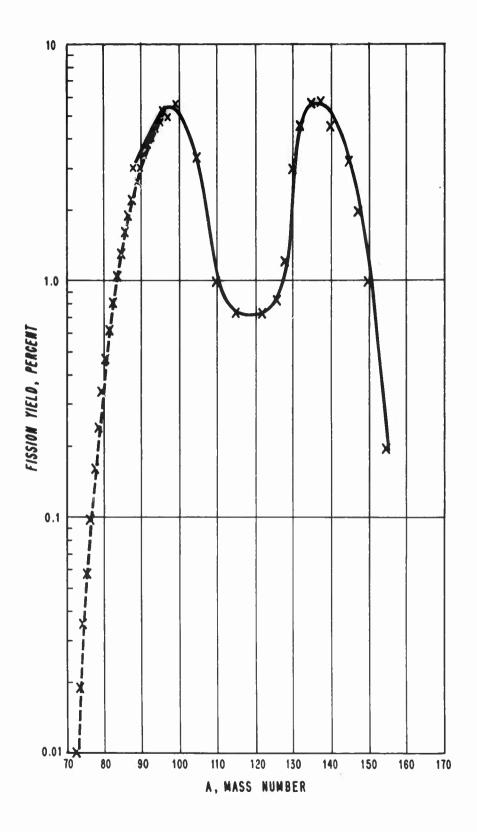
	A 72	2 20	LAMBO	FU238	Fuz35	E0	1000000051	Forbidden O	91	Z 36	LAMBO 7070000049	FU238	FU235	7200(
	72	20	6930000049	2900000046	6960000043	1780000082	1000000051	ó	91	37- 37-	6930000048 6930000048	1700000048	3720000048 558000J048	9200(
	72	30	3930000045	1000000046	3600000043	3200000050	9500000050	0	91 91	37	8250000047	34000000048	7360000048	60000
•	72	31	1350000046	1400000044	2200000042	1280000081	4200000050	0	P1	38	1990000046	6120000047	3060000048	40600
						3020000051	1000000000	0						27200
						806 0000051 634 00000051	8000000049	0						21800
	73 73	20	3460000050	2500000046 4600000046		1900000052	1000000051	0	91 92	39 35	1380000044	5000000044 4620000048	3900000048	30806
•	73	30	1540000049	2600000046	4 320000044 3180000044	9300000051	100000001	0	92	34	2310000050	1550000049	1990000049	91406
	73 74	31 20	3850000046 4620000050	2600000045	4800000043 2200000044	2809090051 1439000052	100000001	0	92	37 38	7400000046	1370000049 3140000048	2430000049 9600000048	11000
	74 74	29	1730000050	7800000046	9100000044	2090000052	1000000051	0	92	39	9350000046	4100000044	1000000047	72006
	74	30 31	1480000048	7200000046 1800000046	1020000045 3380000044	4800000051	3330000051	0	72	30	12,000000	410000004	30000000	54004
						4000000051 2200000051	3330000050	0	93	36	3460000050	1500000049	1210000049	10000
	25	29	2770000050	1100000047	2820000045	1590000082	1000000051	0	93	37 36	1410000049	18000000049	2590000049	12200 87400
	76 75	30	7290000049 9900000048	1600000047	4360000045	650000051	1000000051	0	93	39	1850000046	1400000047	2900000048	57600
	75	25	1410000047	2800000045	2300000044	1280000051	1500000050	0						52000 38800
	76	29	3460000050	1100000047	3890000045	2390000052	1000000051	0						29600 14800
	76 76	30	2310000049	2700000047 1800000047	7660000045 7890000045	790000051 1460000052	1000000051	0	94	36	4950000050	9700000048	4200000048	11900
	77 77	30	4620000050	7800000046 3620000047	5300000045 2190000046	158-000052	1000000051	0	94	37 38	2310000050	1980000049	2130000049	19580
	77	31	4620000049	4120000047	2450000046	1000000052	1000000051	0	94	39	7000000047	1720000048	1020000049	10800
	77 77	32- 32	140000049	7620000046	4100000045	5460000051 4390000051	1000000051	0	95 95	36 37	6930000050 3460000050	1790000049	4570000048 1500000049	19600
						2760000051	3500000050	Ó	95	38 39	1650000049	1930000049	2740000049 1830000049	12000 64800
	77	33	494 000 0045	1100000045	2000000044	1420000051	2300000050	•	95	40	1230000044	3500000046	2200000048	72000
	78 78	30 31	2770000050 8660000049	4720000047 7360000047	4230000046 6540000046	1120000052	1000000051	0						17800
	78 78	32	1340000047	3680000047	3890000046	1800000051	100000001	0	95	41-	2140000045			31600
		33	1270000047	2400000046	3500000045	2800000051	7000000050 3000000050	0	96	37	6930000050	1570000049	5700000048	22900
	79 79	30 31	4620000050	3500000047	64000000046 1600000047	1922000052	1000000051	0	76	38 39	2770000050 6930000049	2350000049	2340000049 2620000049	78000 15500
	79 79	38	2770000049	8400000047	1300000047	1014000052	1000000081	•	97 97	37	4020000050	8280000048 2380000049	9200000048	18700
	80	30	4420000050	2080000047	2600000046 4900000046	1444000051	1000000051	0	97	39	1390000050	1840000049	2790000049	12340
	80	31	2310000060	1490000048	2470000047	2140000052 5480000051	1000000051	0	97	40	1130000046	3510000048	1650000049	92000
	80	33	1920000049	5440000047	1190000047	1100000052	1000000051	•	97	41-	1140000049	7500000045	7000000047	
	01 01	31 38	3460000050 9900000049	2160000048	4230000047 6540000047	1708000052	1000000051	0	97	4 L 36	1560000047	8190000048	7000000047 6800000048	10940
	81 81	33	1390000049	1320000048	3890000047	850000051	1000000051	0	**	39	2770000050 4420000049	2430000049	2420000049	35000
	01	34	6420000047	1410000047	1700000046	2760000051	1000000051	0	98	41	4440000047	4240000048	6800000048	11200
	82	31	4620000050	1200000048	3840000047	2534000052	1000000051	0	••	39	4620000050	2170000049	1690000049	15400
	A 02	2 32	LAMBO 1390000050	FU238	FU235	950000001	1000000051	Forbidden O	9 0	40	2310000049	FU234	FU235	102001
•	92	33	3650000049	1920000048	1020000048	1662000052	1000000051	o	79	41	3040000046	9700000048	1550000049	64,000
	83	32	3460000050	3220000048	1840000048	1700000052	1000000051	0	••	42	2920000045	2000000047	1400000048	160001
	0.3	34-	7700000047	5720000047	5000000047	3000000051	1000000051	0	100					82000
	83 83	34	1400000048	7280000047 1800000046	4000000047	1860000051	1000000051 8000000050	ô	100	39 40	1980000090	2600000049	7800000048 2330000049	700000
	84	38	4620000050 2770000050	3240000048	3460000048	1222000052	1000000051	0	100	41	2570000049 6930000050	1580000049	2080000049	147000
	84	34	3500000048	2310000048	2540000048	2600000051	1000000051	0	101	40	2770000050	2180000049	1790000049	132000
	84	38	3610000047	1150000047	3800000047	9360000051 7120000051	900000000	0	101	41	6300000049 7910000047	2010000049 4900000048	2120000049 9600000048	112000
						3440000051	1600000050 3500000050	0	101	43	8250000047	2100000046	3000000047	240000
	85	38	6930000050	2010000048	1440000046	1946000052	1000000051	0						210000
	85	33 34	1610000051	5720000048 4420000048	5080000048	1464000052	1000000051	0	102	40	3460000050 9900000049	1770000049	8500000048 1810000049	173800
	85	35	3850000048	8450000047	1440000048	1000000051	7700000051	0	102	42	13900000048	9500000048 2450000047	1330000049	254000
	85	34~ 34	4380000046 2130000042	3000000044		1390000051	9900000000	i	103	40	4620000050	8580000048	3700000048	157400
	86	32	6930000050	1420000048	1578000048	3000000050	100000001	0	103	41	1730000050	2030000049	1330000049	136200 870000
	84	33	3460000090	5440000048	5640000048	2248000052	100000001	0	103	43	9620000048 2020000044	2110000048	3700000048	
	84	34 35	4060000049 2170000049	2240000048	8720000048 5180000048	6780000051 1412000052	1000000051	0	*	44		3700000045		137000
	87 87	33	4620000050	1700000048	1150000049	1834000052	1000000051	0	103	45	2030000047 4620000050	3670000044	4078000048	122400
		35	1250000049	7704000048	1020409049	1200000051	7000000050	0	104	41	2310000050	1520000049	6800000048	199600
	A7	36	1480000047	200000048	2500000048	1600000052	7000000050	0	104	43	3850000049 6420000047	4800000048	9100000048 4700009048	600000
						2600000051	2500000050	0	105	41	1160000050	9670000048	2366000048	163600
	44	34	2770000050	6820000048	1140000049	1048099052	1000000001	0	105	43	1160000048	7820000048	4802000048	9440001
	88	35 36	4470000049	1010000049	7900000049	1794000082 5600000081	2000000000	1	105	45-	1340000046	5100000047	9520000047	230000
						1800000051	1200000050		105	45	23100000090			114000
	88	37	64900000047	2420000047	5000000047	1024000052	6609000050	0	106	41	4620000050		6160000047	2240001
						4000000051	1900000050	0	106	42 43		9160000049	2870000048	788°000
	89	34 35		4850000048 140000049		1388000052	1000000051	0	106	44	2200000043	1760000048	9520000047	7800000
	89	36	3630000046	8320000048	1580000049	8000000051	1000000051	ó						4600000
	89	37	7500000047	1430000048	3100000048	7840000051 5600000051	70000000049 5000090049	ŀ	107	41	6930000050 2770000050	1210000048 7140000048		1382000
		36	1590000044	2900000045		2950000051	1000000050	G 1	107	43	1920000047	9240000048 336000		-
	90	34	6930000050	2350000046		1374000052	1000000051	0	107	45	4610000047	46000	4	
	90	36	4950000050 2100000049		2200000049	6404000051	1000000051	0	107	46	5420000047 3460000050	36700	1	
	90	37 38	4220000048 7930000041	4200000046	10000000049	114000052	1000000051	0	108	43	1980000050	705000 39000	100 m	ŀ
	90	39	3000000045			4520000051	9900000050	1	108	45	3850000049	37500	_	- 1
•	91	35	3460000050	7930300048	8280000048	1714000052	100000001	0	109	42	4620000050	12900	_	1
														1
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														لـــــــــــــــــــــــــــــــــــــ

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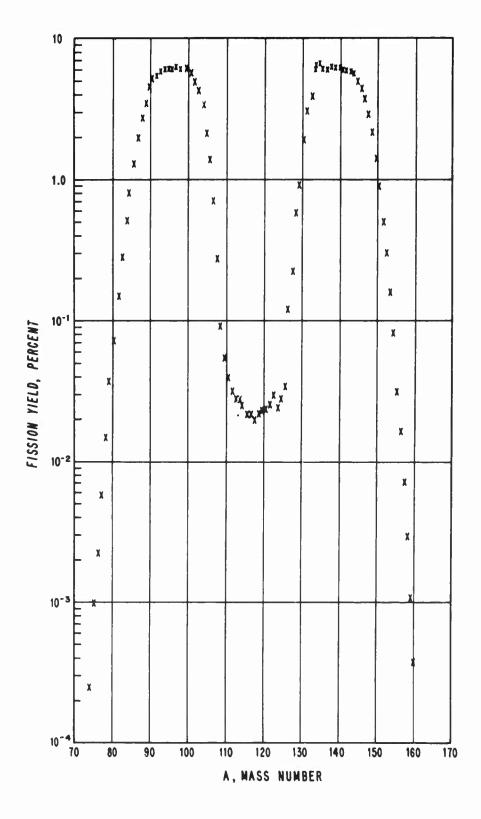
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2	1000000051	ě	91	37-	6930000048 6930000048	1700000048	3720000048	9200000081	1000000081		109	44	4330000049	1000000048	2300000047 7600000046	9220000051 7080000051	1000000
	9500000050 5000000049	0	91 91	37	8250000047	3400000048	7360000048	400000001	1000000081	1	109	46	1380000046	4400000045		200000001	9900000
	4200000050 3100000050	0	♥1	36	1990000046	6120000047	3060000048	5340000051 4060000051	2600000050	i	110	42	6930000050 3460000050	4600000047 2920000048	1300000047	1215000052	1000000
1	1000000050	ó						2720000051	2900000050	0	110	44	6930000049 3460000049	4230000048	1360000046	1308000052	1000000
1	9000000049 8000000049	0						2180000081 1240000061	3300000050 7000000049		110	45	4620000050	1610000048	5400000046	1400000052	1000000
2	1000000051	ŏ	91			5000000044		3080000681	1000000091	I O	111	44	1730000050	3780000048	1 300000047	1108000052	1000000
2	1000000051	0	92	36	4620000080 2310000080	4620000048 1550000049	1990000049	9140000051	1000000051	ě	111	46	4440000047	2610000048 3950000047	2180000046	4300000051	1000000
1	1000000051	0	92	37	8660000048	1370000049	2430000049	1674000052	100000001	0	iii	47	1060000045	6000000044		206 ⁰ 000051	1000000
2	1000000051	0	92	30	7400000046	3140000040	9600000048	3000000051	1000000050	è						1400000051	80000006
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1	3330000050							2400000051	3300000050	0	112	45	9900000049	3200000048	1146000047	1490000052	10000000
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	9900000050	1	108	45	3850000049	3750000047 1290000048	6300000046	120000000	1000000051	0	129	40 50	4620000050	7230000048	3920000		/ 1
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0	109	43	2770000050	4520000048	2040000047	1416000052	1000000051	0	129	51	4580000046	7540000048	2020000048	3740000051	2000000050
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ō	iii	47	1060000045	6000000044	2,0000000	2080000051	9100000080	¥.	1 30	9:	1630000048	1370000049	3040000048	1150000052	100000001
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	113	46	8250000048	1700000048	6300000046	702000001	100000001	•						1214000081 6700000080	872000050 9300000049
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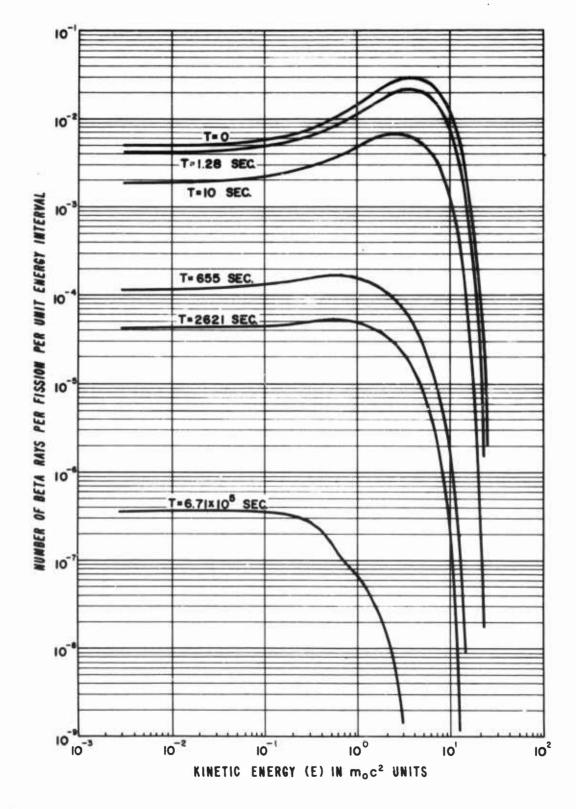
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		Fugae	Fuzas	EO	Δ	Forbidden	A	2	LAMOD	Fugae	Fuzas	20	Δ	Forbidden
51	4580000046	7540000048		3740000081	2000000000	.0		_		10236	. 0230	4004000050	60000000049	0
				3400000051	2000000050	0	143	59	5830000044 4620000050	4720000048	6800000048	1546000051	1000000051	0
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51	1630000048	1370000049	6040000048	1158000081	1000000051	o	145	54	3460000050	9280000048	1430000049	1014000052	1000000081	ě
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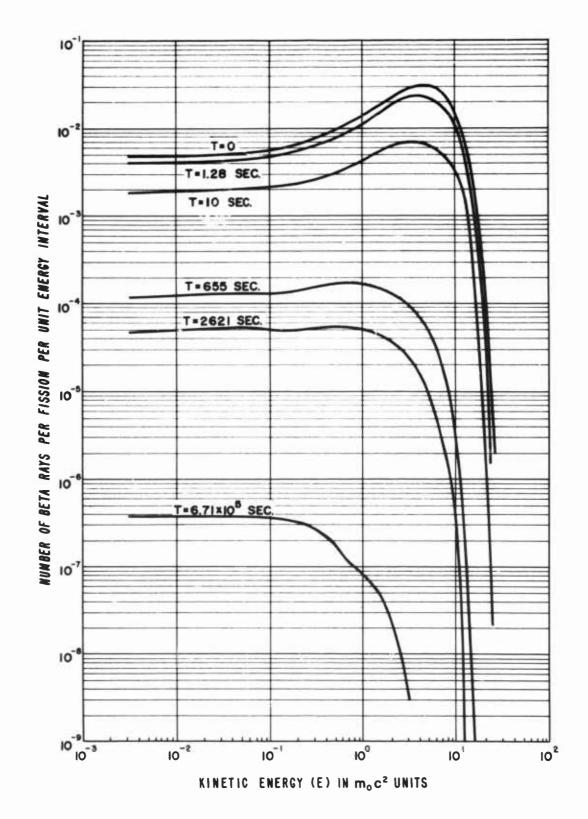


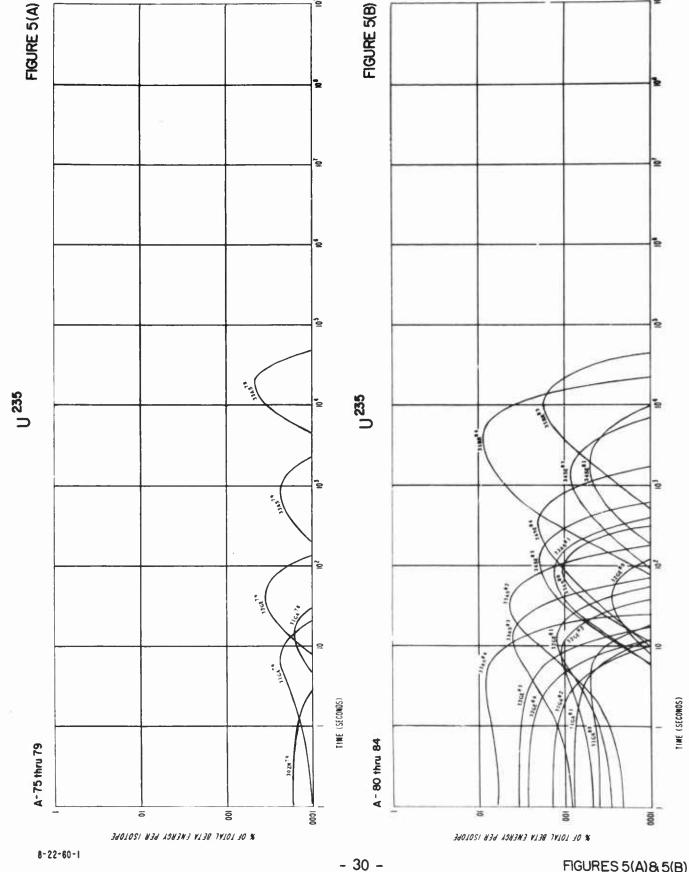
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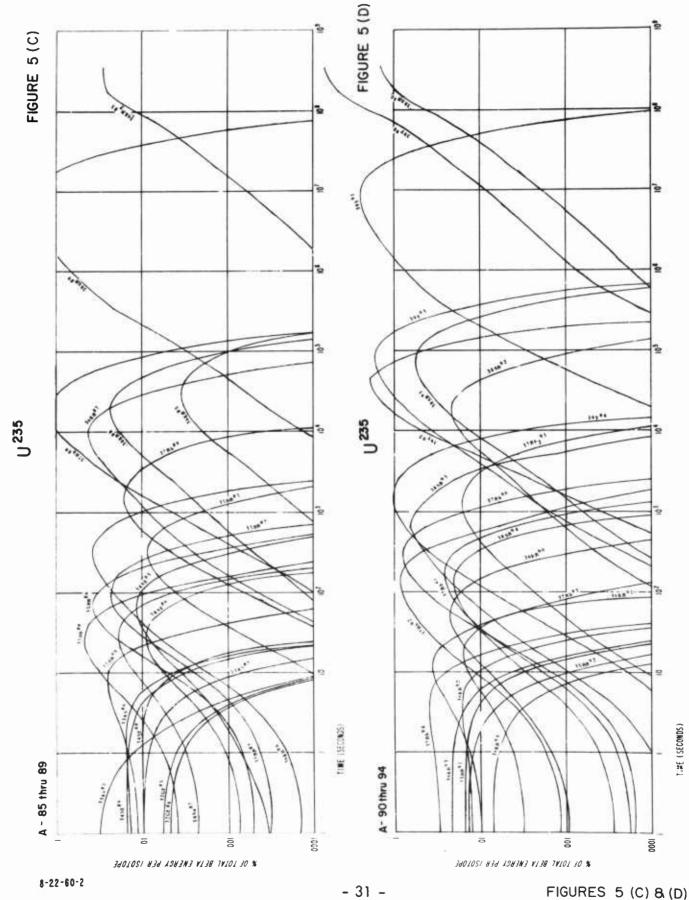


THE BETA RAYS FROM U 235 FISSION BY FISSION SPECTRUM NEUTRONS

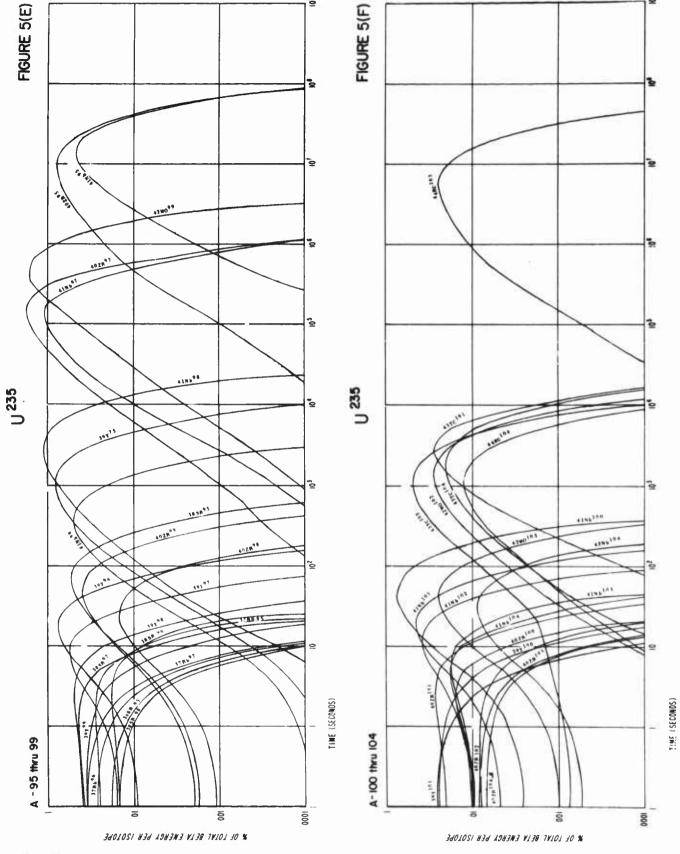




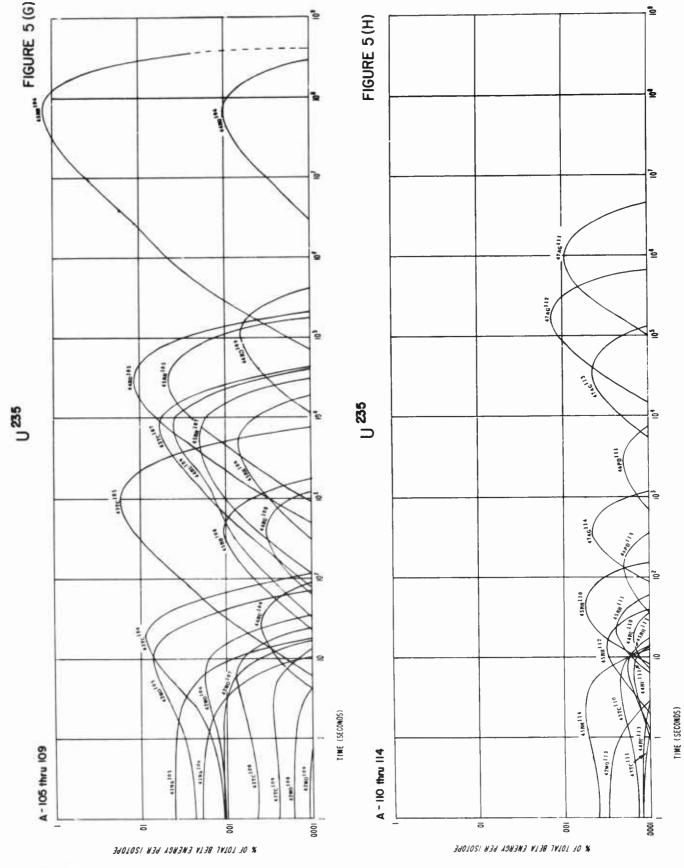


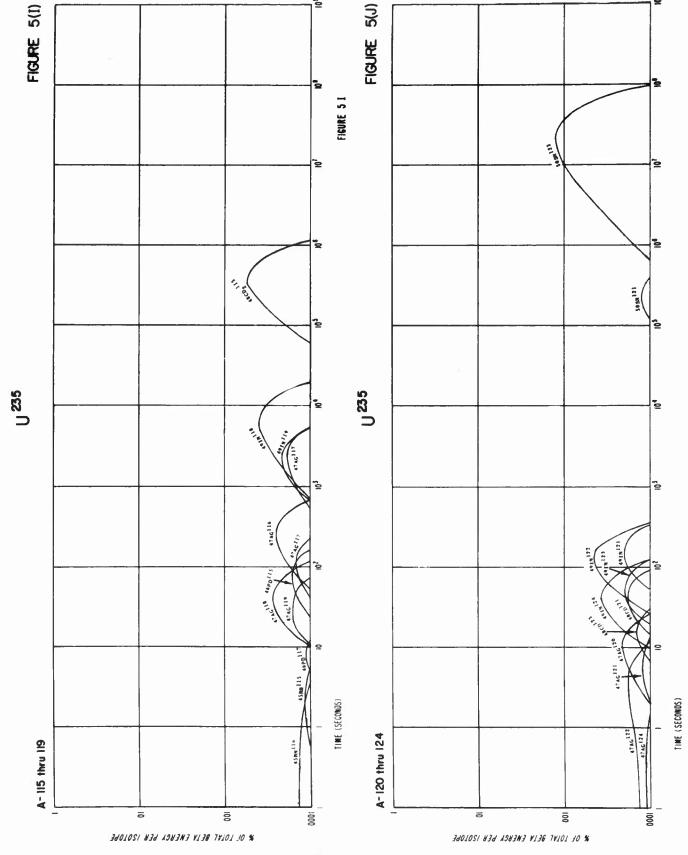


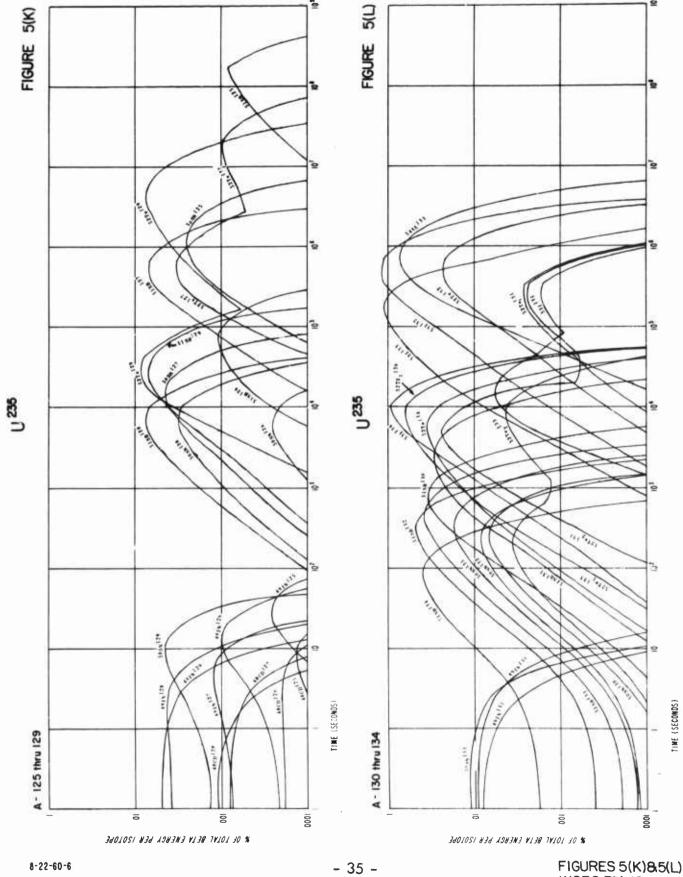
FIGURES 5 (C) 8 (D) WSEG RM 19



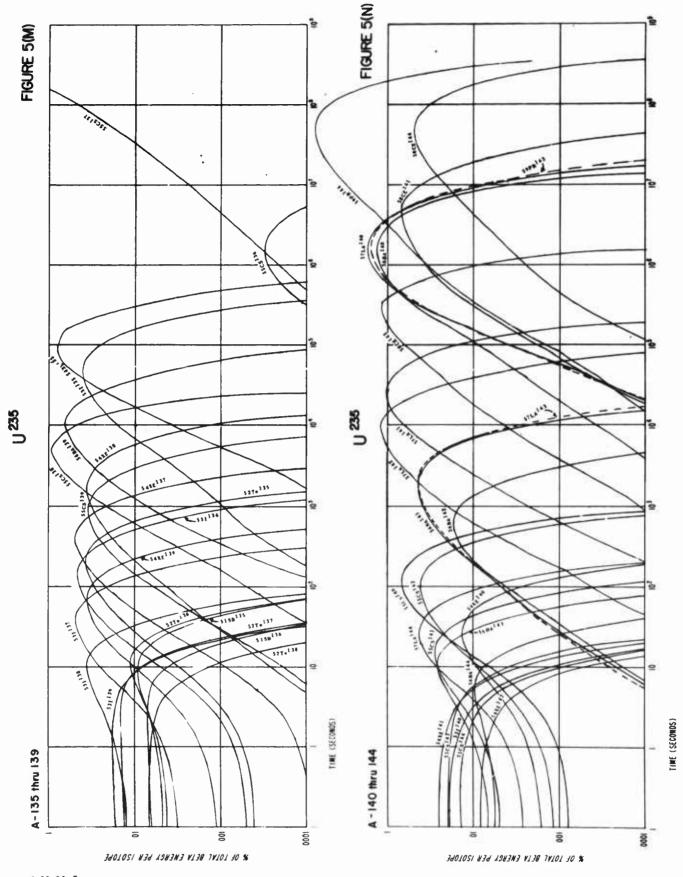
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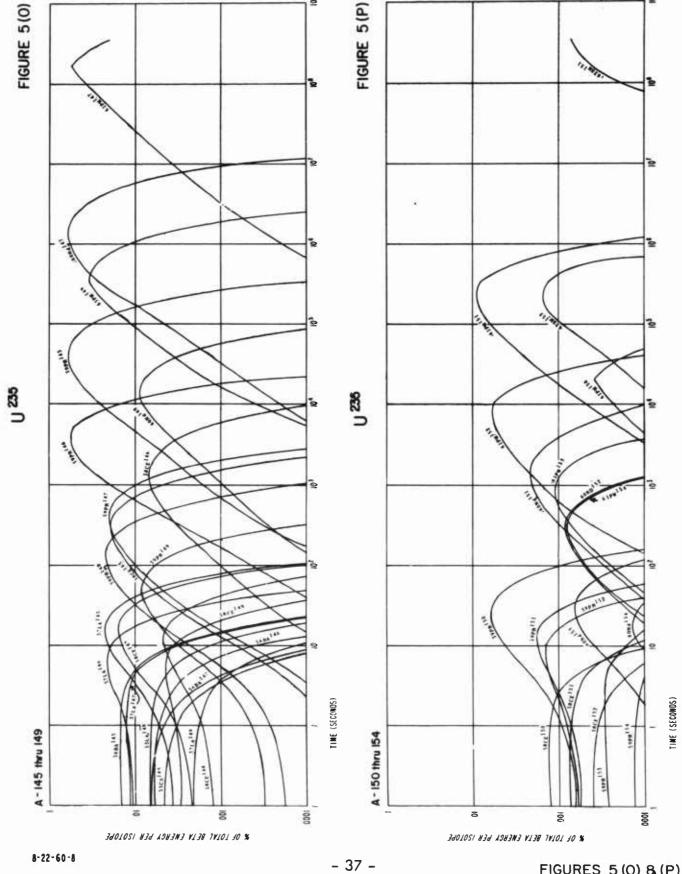


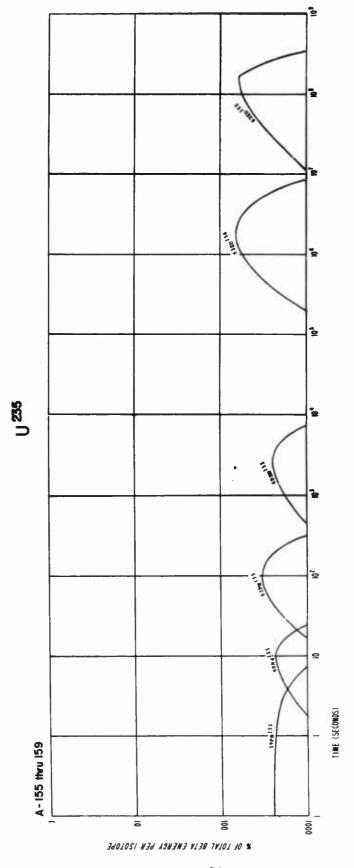


FIGURES 5(K)&5(L) WSEG RM 19



8-22-60-7

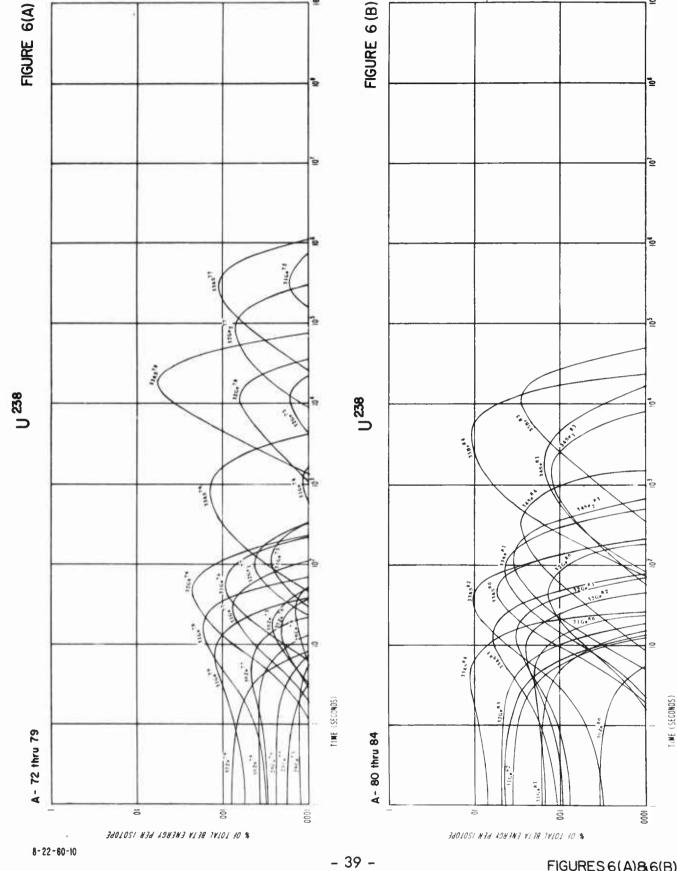


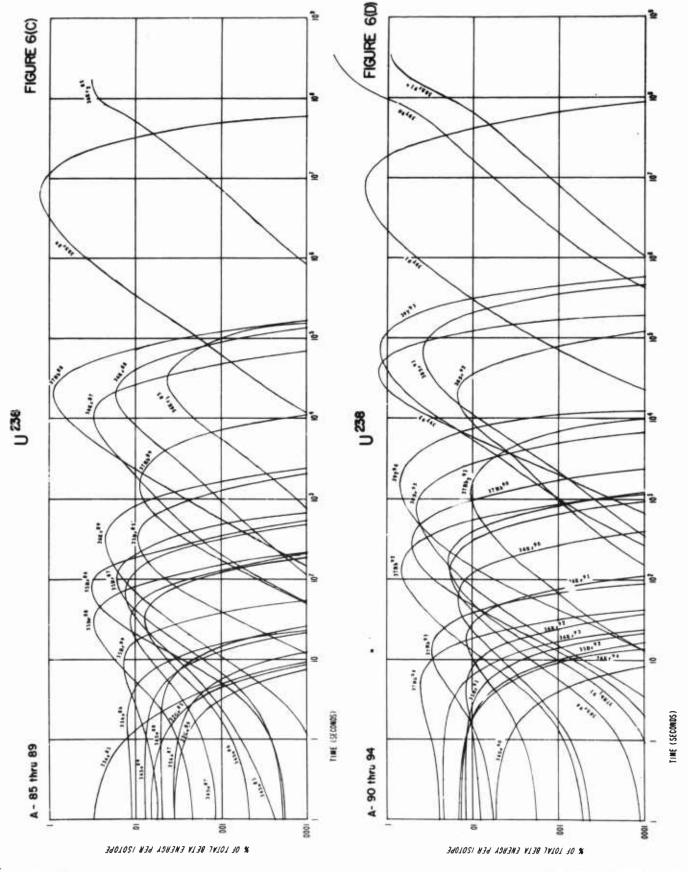


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FIGURE 5 (Q) WSEG RM 19

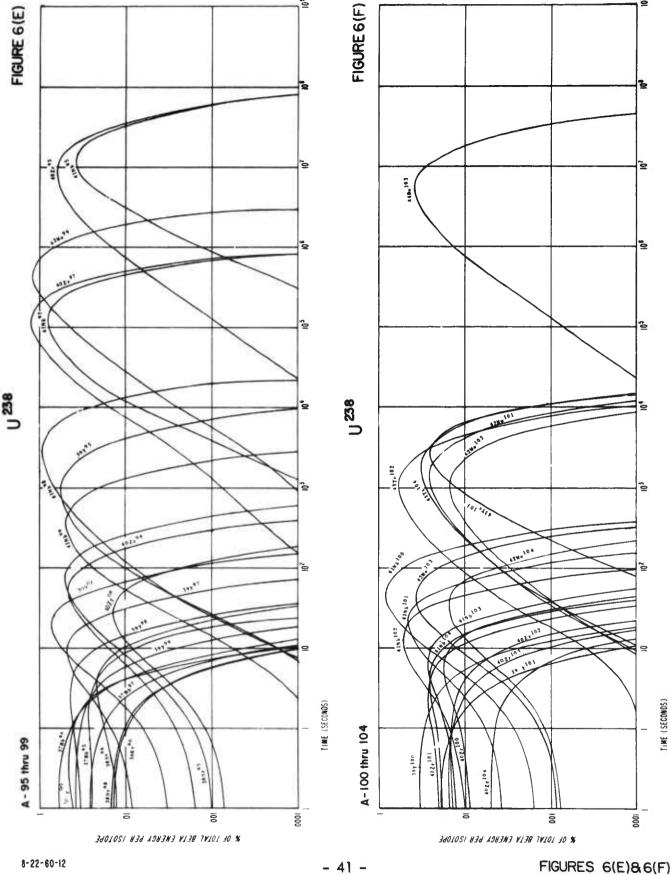




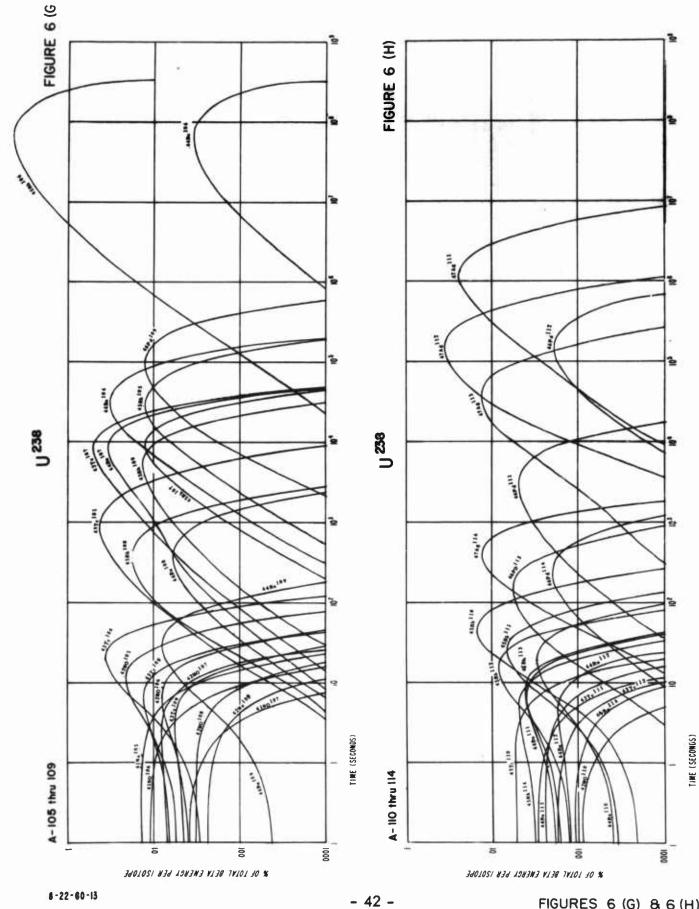
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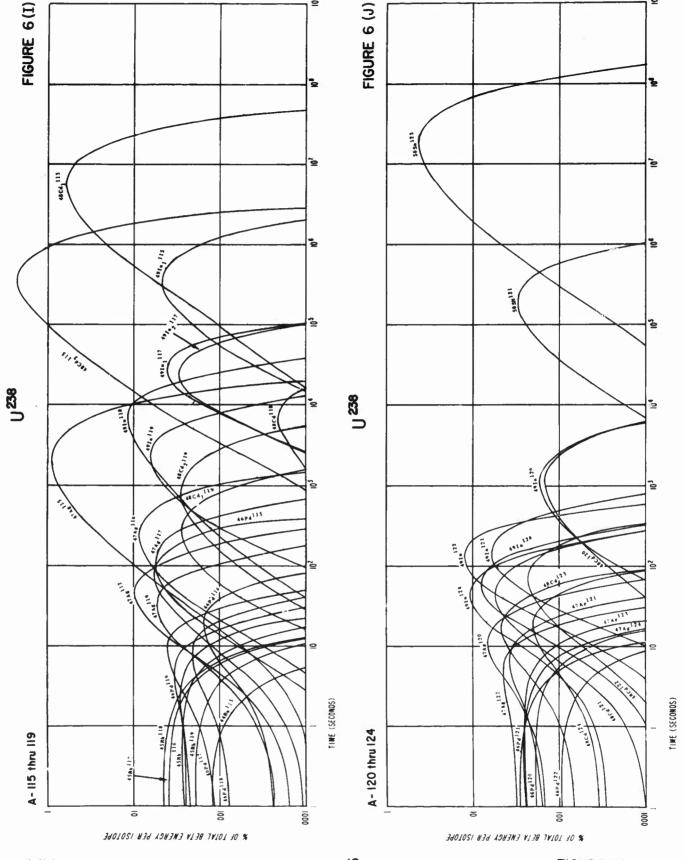
FIGURES 6(C) & 6(D) WSEG RM 19

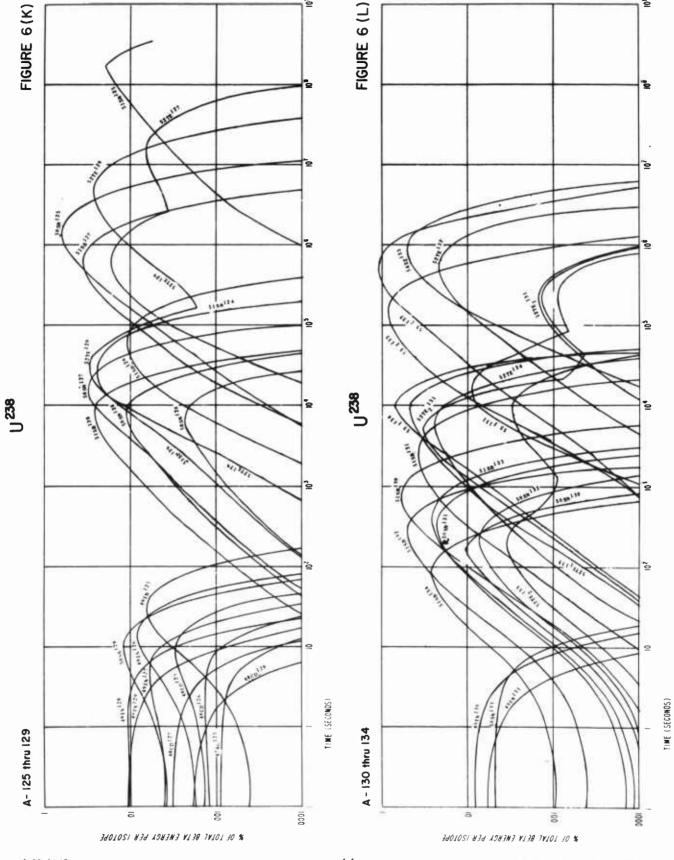


FIGURES 6(E)&6(F) WSEG RM 19



FIGURES 6 (G) & 6 (H) WSEG RM 19

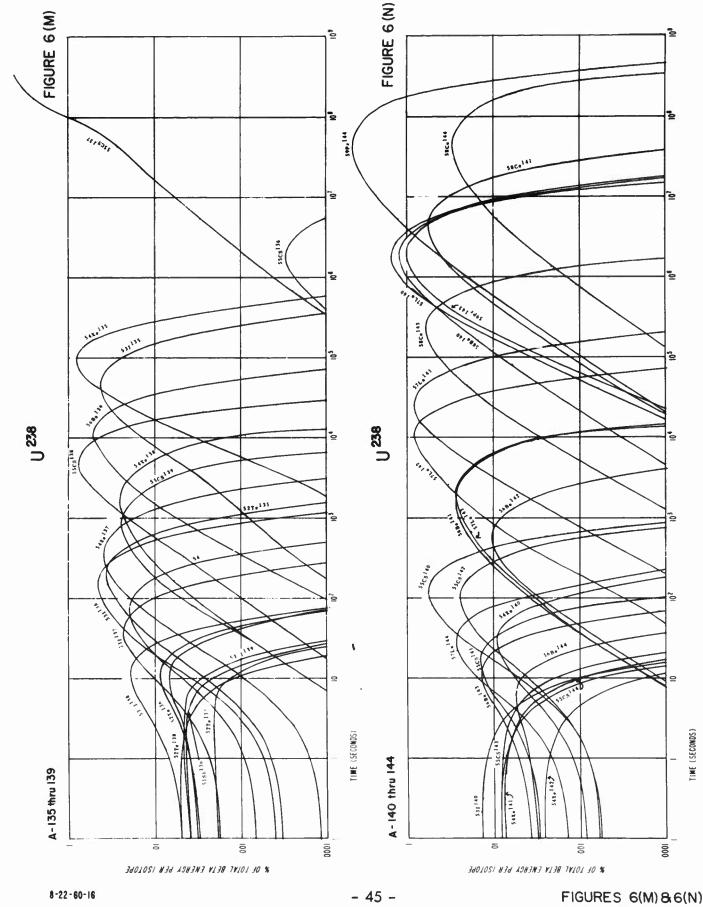


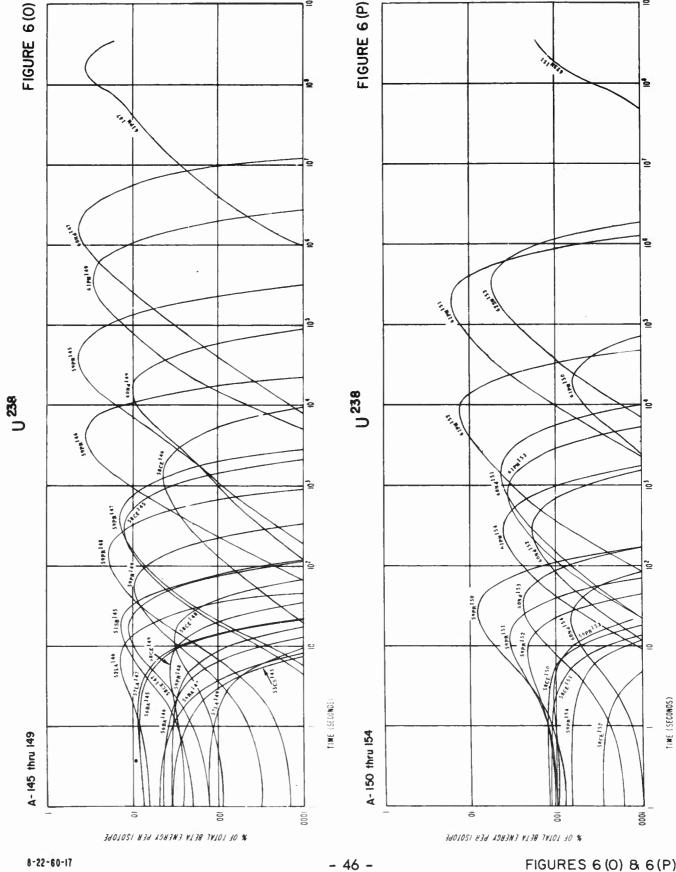


8-22-60-15

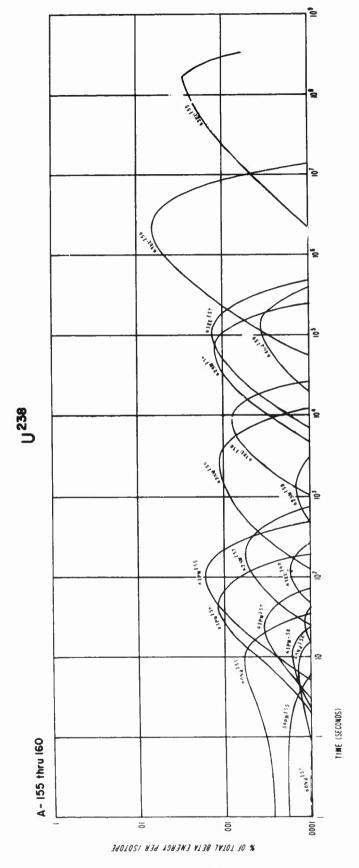
- 44 -

FIGURES 6(K) & 6(L) WSEG RM 19

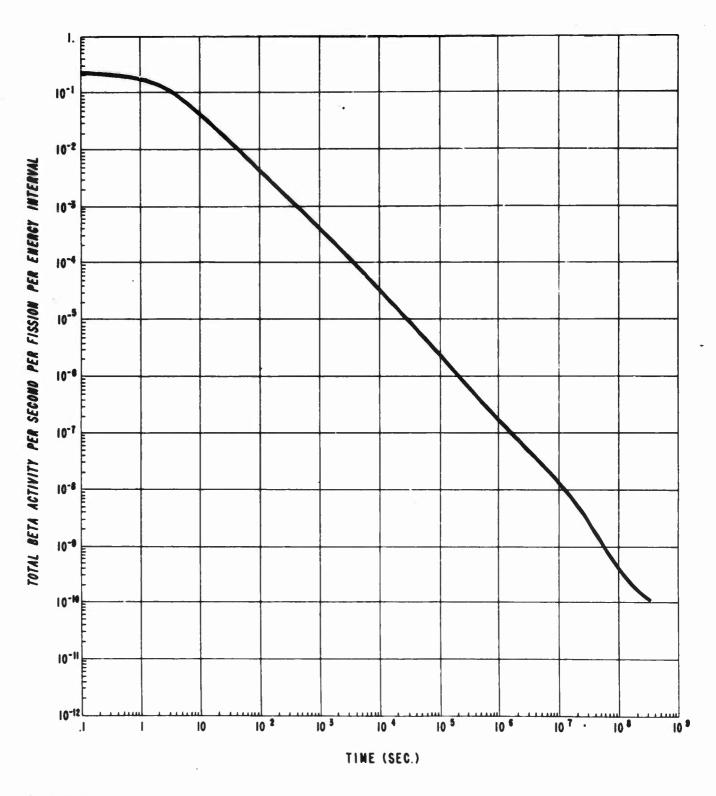




FIGURES 6 (O) & 6 (P) WSEG RM 19



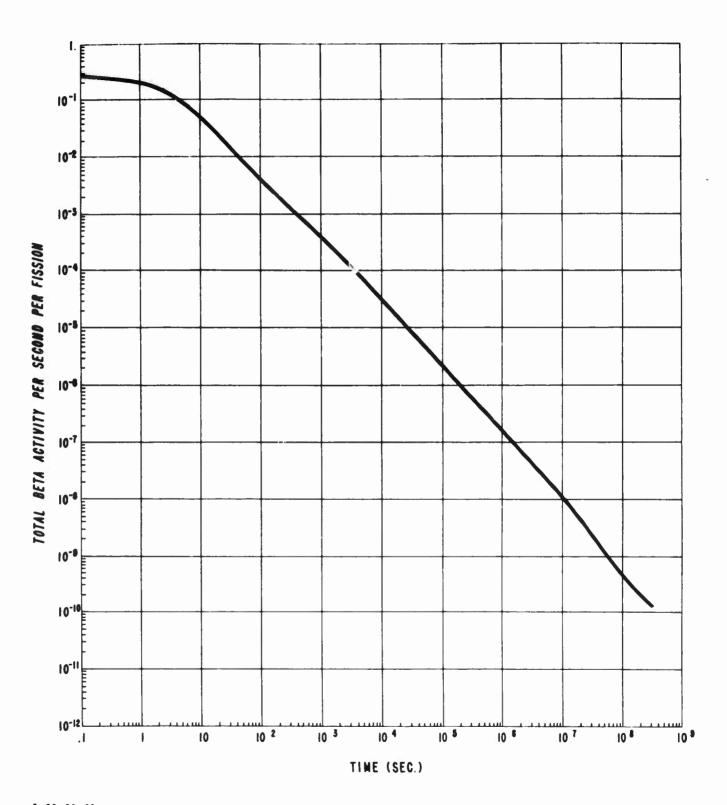
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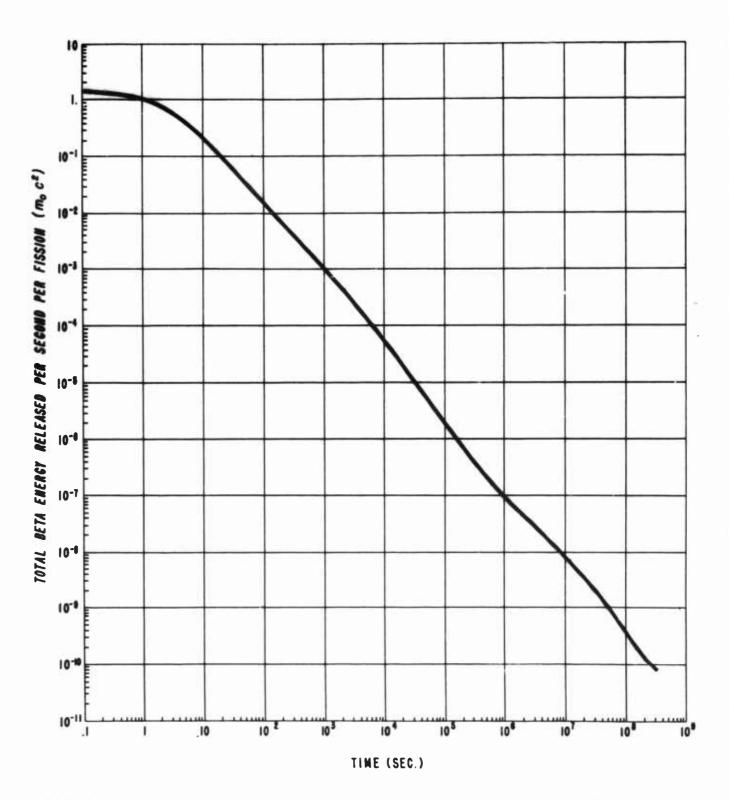
8-22-60-19

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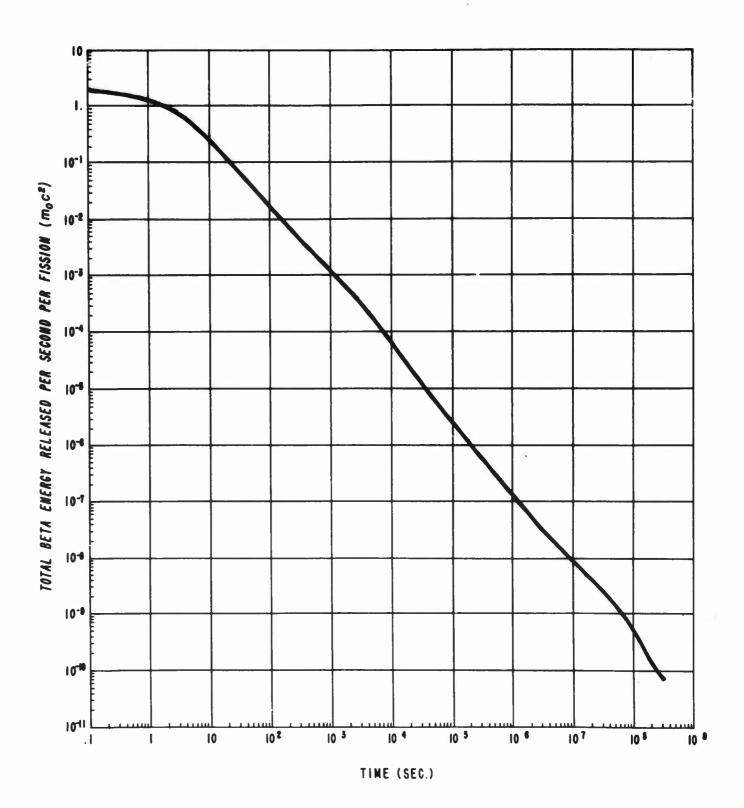
FIGURE 7 WSEG RM 19



8-22-60-20



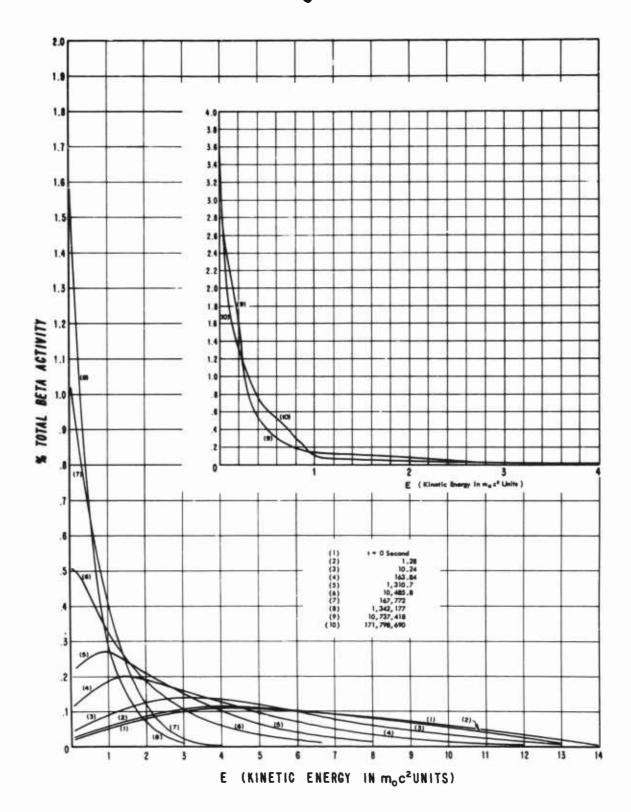
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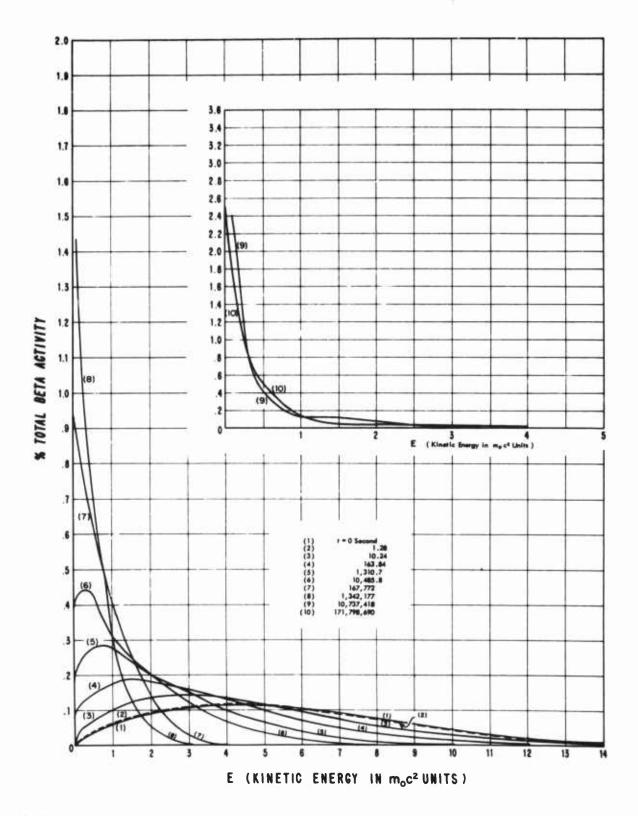


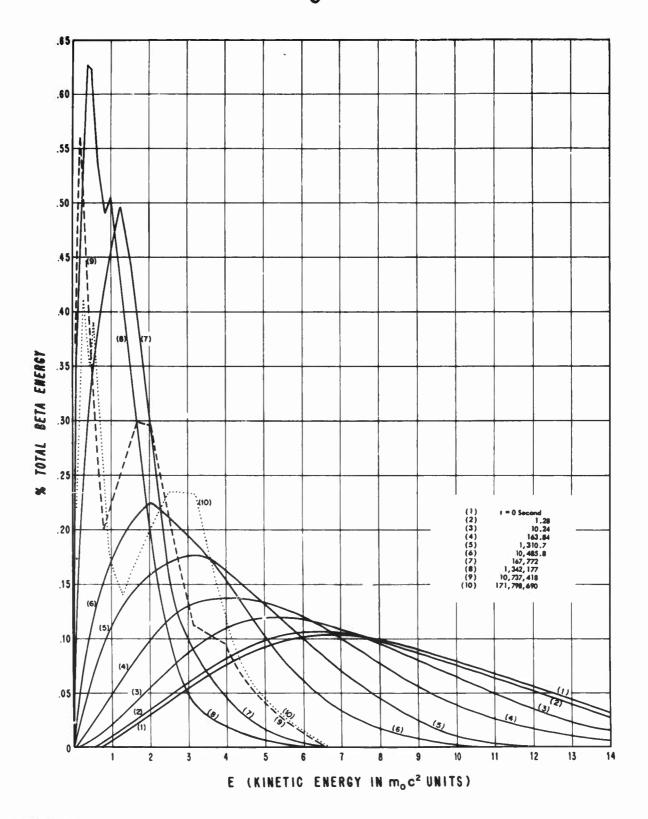
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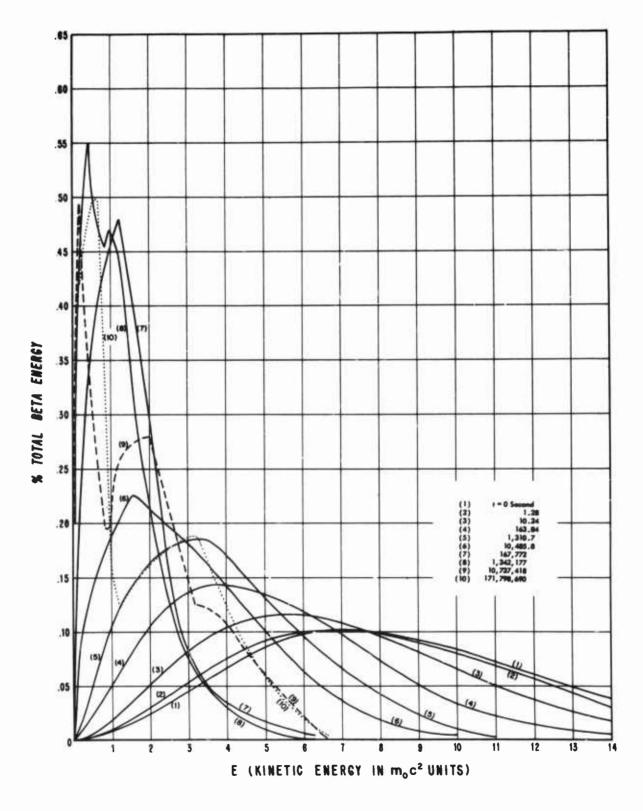
- 51 -

FIGURE 10 WSEG RM 19

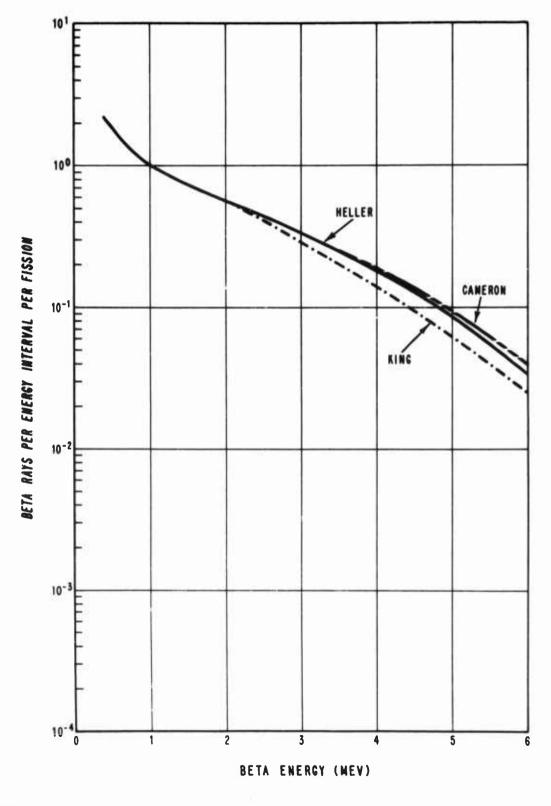








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